

BS4142 ASSESSMENT OF
EXTRACTION SYSTEM AT
209 NEW ROAD,
SKEWEN,
NEATH,
SA10 6ET

April 30th 2025

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1.0 Introduction

- 1.0.1 This report has been commissioned to determine the noise impact of the plant noise from the proposed extraction system at 209 New Road, Skewen, Neath, SA10 6ET.
- 1.0.2 The assessment has been conducted in line with the BS4142:2014 in order to assess the industrial sources with the potential for noise impact on surrounding residential properties.

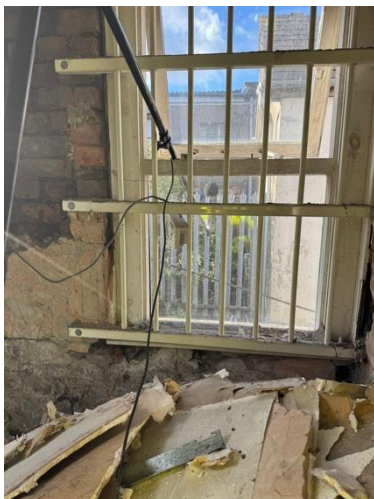
2.0 Site Details

- 2.0.1 The extraction system is to be located at the rear of the proposed takeaway unit on New Road, Skewen. The assessment has been conducted to assess the impact of this proposed system on the surrounding residential Noise Sensitive Receptors (NSRs).
- 2.0.2 The closest Noise Sensitive Receptors (NSRs) are located on the rear façade at first-floor level along New Road.
- 2.0.3 The noise sources is not currently in situ and therefore background noise levels were taken at the site. This included other industrial noise from surrounding AC and extraction systems from existing retail units, restaurants and takeaways.

2.1 Location of Monitors

- 2.1.1 The noise location was chosen based on the proximity to the closest NSR.

Figure 1 – Reception/NSR Boundary



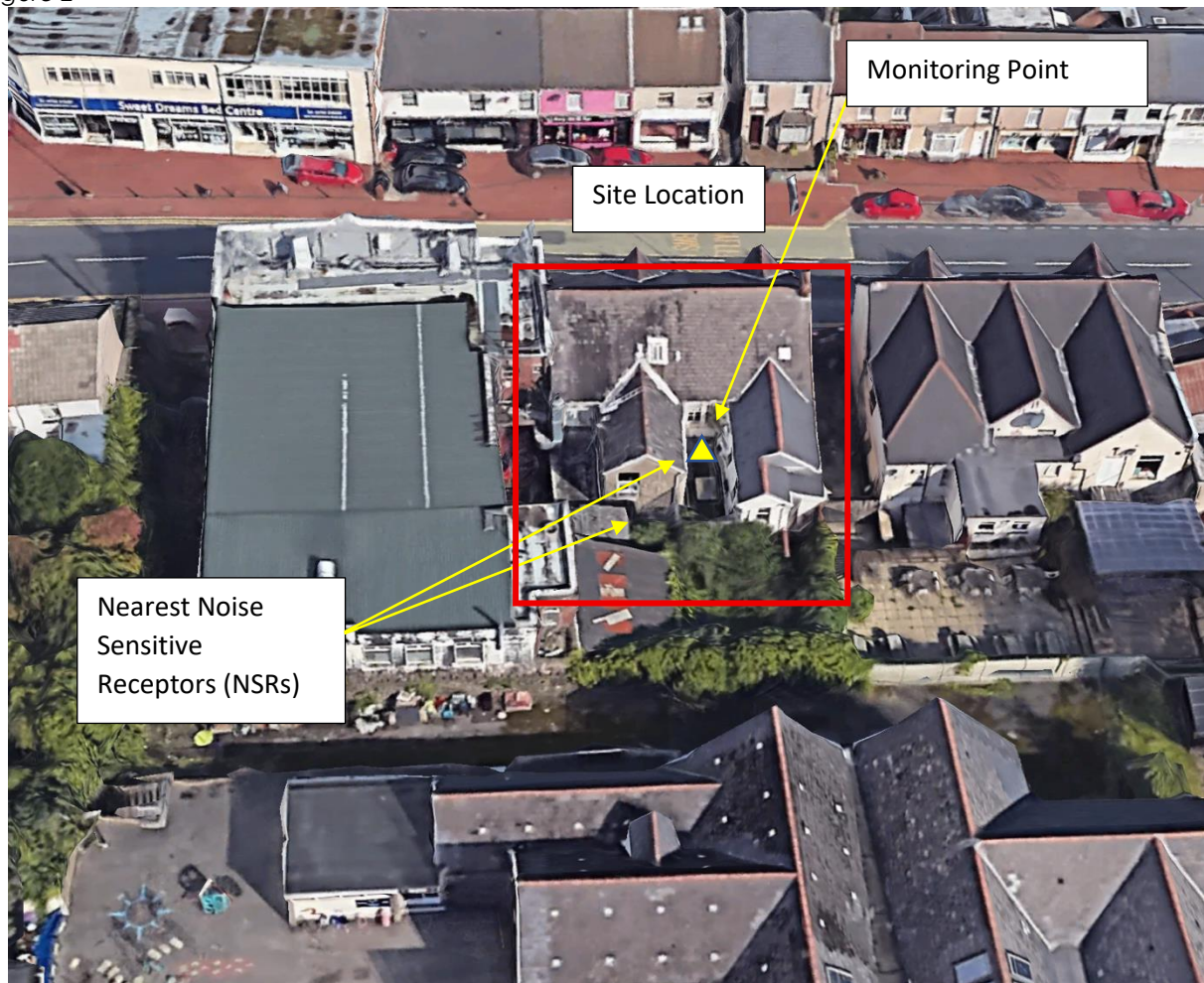
- 2.1.2 Measurements were made in 15 minute periods, on 1 second averaging, to allow for the removal of anomalies and increased accuracy. The data was averaged into L_{Aeq1hr} daytime and $L_{Aeq15min}$ night-time with data also

recorded for L_{A90} in both day and night periods for the BS4142:2014 assessment.

- 2.1.3 The monitoring was conducted using 1 x Type 1 Nti XL2 sound level meter with batteries and outdoor microphone protection.
- 2.1.4 All measurements were taken after a field calibration was undertaken to ensure accuracy and repeatability of measurements. Drift was also checked post-measurement to validate the data collected.
- 2.1.5 Further data such as wind speed, wind direction, rainfall intensity, temperature and cloud cover were all recorded at the beginning and end of the assessment at the monitoring location.
- 2.1.6 Any anomalies (such as noise by the engineer during setup and collection of the kit) were removed from the survey for a true reflection of the ambient levels in the vicinity. This was done by recording audio throughout the survey at each location and listening back through the files during the analysis process to confirm what was recorded manually during the survey.

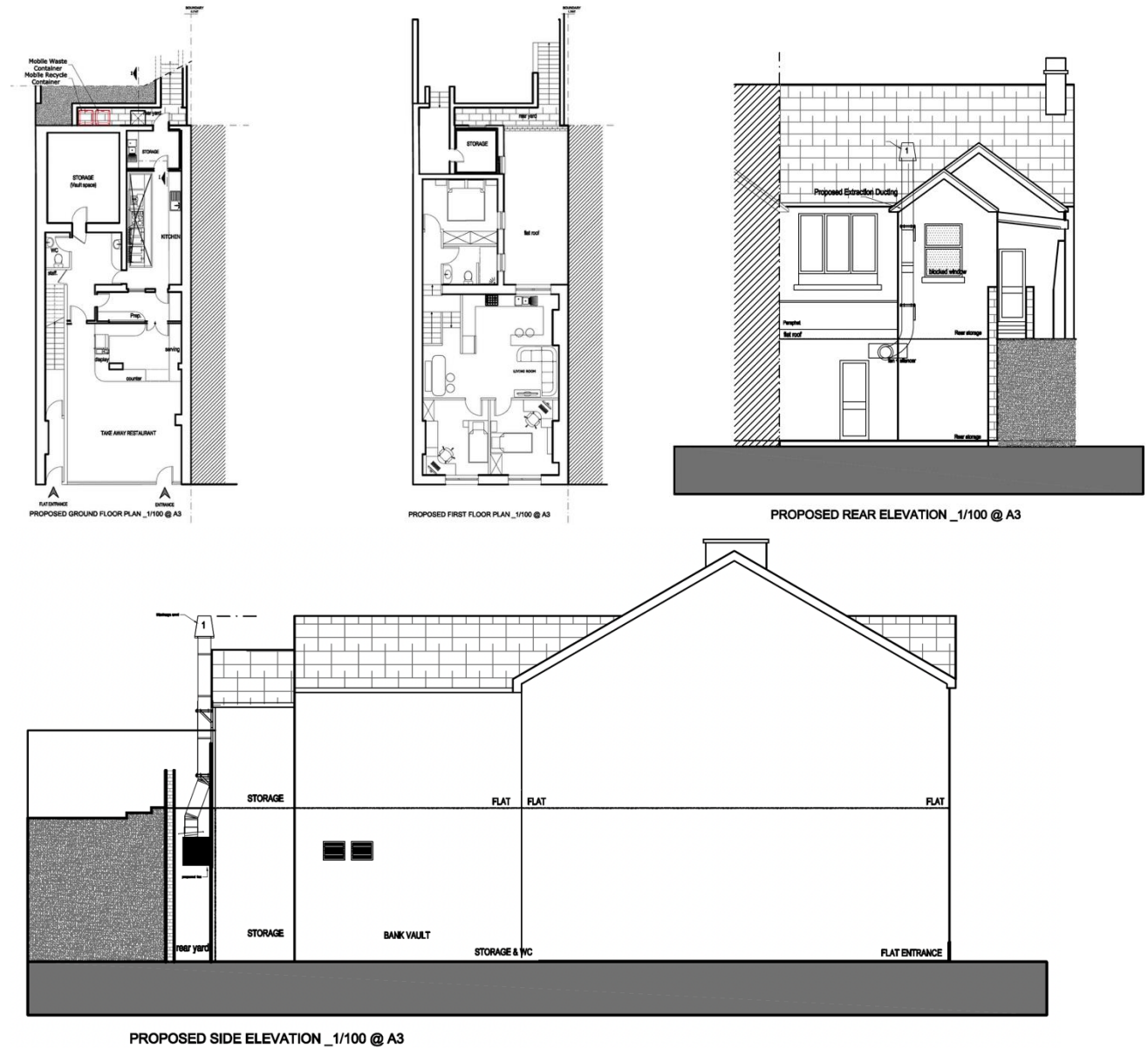
2.2 Plan Views of Site with Designated Work Areas

Figure 2



2.3 Proposed Extraction Location

Figure 3 – proposal drawings



3.0 Legislation

Legislation - National Planning Practice Framework

- 3.0.1 The Planning Policy Wales sets out the Government's economic, environmental and social planning policies. Section 3.22 states;

"Planning authorities should develop and maintain places that support healthy, active lifestyles across all age and socio-economic groups, recognising that investment in walking and cycling infrastructure can be an effective preventative measure which reduces financial pressures on public services in the longer term. The way a development is laid out and arranged can influence people's behaviours and decisions and can provide effective mitigation against air and noise pollution."

- 3.0.2 The guidance also sees traffic consideration and management as key when it comes to noise impact assessments. Section 4.1.45 states

"Local authorities must adopt an integrated approach to traffic management. They should consider how different measures can complement one another and contribute to the achievement of wider planning and transport objectives, implementing the Active Travel Act and reducing exposure to air and noise pollution, taking into account the needs of the disabled and less mobile sections of the community."

- 3.0.3 Section 6 of the document also tackles the likely social and well-being impacts of the preservation of 'distinctive and natural places'. Section 6.7.1 refers to the need to protect the soundscape of areas;

"Clean air and an appropriate soundscape, contribute to a positive experience of place as well as being necessary for public health, amenity and well-being. They are indicators of local environmental quality and integral qualities of place which should be protected through preventative or proactive action through the planning system. Conversely, air, noise and light pollution can have negative effects on people, biodiversity and the resilience of ecosystems and should be reduced as far as possible."

This is then continued in reference to noise in section 6.7.4;

"The planning system should maximise its contribution to achieving the well-being goals, and in particular a healthier Wales, by aiming to reduce average population exposure to air and noise pollution alongside action to tackle high pollution hotspots. In doing so, it should consider the long-term effects of current and predicted levels of air and noise pollution on individuals, society and the environment and identify and pursue any opportunities to reduce, or at least, minimise population exposure to air and noise pollution, and improve soundscapes, where it is practical and feasible to do so."

3.0.4. It is possible to apply objective standards to the assessment of noise and the effect produced by the introduction of a certain noise source may be determined by several methods, as follows:

- The effect may be determined by reference to guideline noise values. British Standard (BS) 8233:2014 and World Health Organisation (WHO) "Guidelines for Community Noise" contain such guidelines.

Another method is to compare the resultant noise level against the background noise level (L_{A90}) of the area. This is the method employed by BS 4142:2014 to determine the likelihood of complaint from noise of an industrial nature. It is best suited to the assessment of steady or pseudo-steady noise.

3.1 BS4142:2014 +A1 (2019)

- 3.1.1 Noise effects on residential properties have been assessed according to the guidance in BS 4142:2014. This standard primarily provides a numerical method by which to determine the significance of sound of an industrial nature (i.e. the 'specific sound' from the proposed development) at residential sensitive receptors.
- 3.1.2 The specific sound level may then be corrected for the character of the sound (e.g. perceptibility of tones and/or impulses), if appropriate, and it is then termed the 'rating level', whether or not a rating penalty is applied. The 'residual sound' is defined as the ambient sound remaining at the assessment location when the specific sound source is suppressed to such a degree that it does not contribute to the ambient sound.
- 3.1.3 According to BS 4142:2014, the background sound levels adopted for the assessment should be representative of the periods being assessed. The standard recommends that the background sound level should be collected from continuous measurements of normally not less than 15-minute intervals. However, the Standard states that there is no 'single' background sound level that can be derived from such measurements. It is particularly difficult to determine what is 'representative' of the night-time period because it can be subject to a wide variation in background sound levels between the shoulder night periods.
- 3.1.4 The method chosen for this section of the report is to use the data collected at the nearest NSR for the day and night periods to provide the ambient and background noise levels. The mode ($L_{Aeq_1hr(Day)}$ and $L_{Aeq_15min(Night)}$) value will then be used for each time period over the course of the measurement as the most appropriate way of creating a representative value.
- 3.1.5 The specific sound levels have been determined separately in terms of the L_{Aeq1hr} during the daytime $L_{Aeq15min}$ during the night-time. Daytime is typically between 07:00 and

23:00 hours and night-time is typically between 23:00 and 07:00 hours, so these periods have been adopted for this assessment.

- 3.1.6 At each of the most likely sensitive receptor locations, the rating level has been determined from the predicted specific sound level. Where it has considered it to be appropriate, a rating penalty has been applied for tonality, impulsivity and/or intermittent specific sounds as described in the commentary to paragraph 9.2 of BS4142:2014. This has been applied with consideration for the main sound sources from site that contribute to the level of specific sound at the receptor location.
- 3.1.7 As per the requirements of the standard, an initial estimate of the impact of the specific sound has been obtained by subtracting the measured background sound level from the rating level of the specific sound. Table 2 provides the initial evaluation of impact following this method.

Table 4

Magnitude	Difference Between rating Level and Background Level	Comments
High	+10dB	Significant Adverse impact Likely
Medium	+5 to +10dB	Adverse impact Likely
Low	0 to +5 dB	Adverse impact unlikely
Negligible	Less than 0dB	Low chance of Adverse Impact

- 3.1.8 Following the initial evaluation of impact, the context of the sound has also been considered, which is a key requirement of the Standard. In evaluation of the context, the following factors have been considered:
- the absolute level of the sound;
 - the character and level of the residual sound compared to the character and level of the specific sound and
 - the sensitivity of the receptor and whether dwellings or other premises used for residential purposes will already incorporate design measures that secure good internal and/or outdoor acoustic conditions.

3.2 TAN 11: October 1997

- 3.2.1 The Technical Advise Note (Wales) 11, Noise – October 1997 provides some further criteria in relation to noise criteria categories for Noise-sensitive developments. These categories have been derived to assist local planning authorities in their consideration of planning applications. These categories are part of Annex A of the guidance document and are displayed in the tables below.

“Local planning authorities should consider whether proposals for new noise-sensitive development would be incompatible with existing activities, taking into

account the likely level of noise exposure at the time of the application and any increase that may reasonably be expected in the foreseeable future. Such development should not normally be permitted in areas which are, or are expected to become, subject to unacceptably high levels of noise and should not normally be permitted where high levels of noise will continue throughout the night.”

Table 2: RECOMMENDED NOISE EXPOSURE CATEGORIES FOR NEW DWELLINGS NEAR EXISTING NOISE SOURCES					
Noise Levels⁽¹⁾ corresponding to the Noise Exposure Categories for New Dwellings L_{Aeq,T}dB					
Noise Source		Noise Exposure Category			
		A	B	C	D
road traffic	0700-2300	<55	55-63	63-72	>72
	2300-0700 ⁽²⁾	<45	45-57	57-66	>66
rail traffic	0700-2300	<55	55-66	66-74	>74
	2300-0700 ⁽²⁾	<45	45-59	59-66	>66

TABLE 1: NOISE EXPOSURE CATEGORIES	
A	Noise need not be considered as a determining factor in granting planning permission, although the noise level at the high end of the category should not be regarded as desirable.
B	Noise should be taken into account when determining planning applications and, where appropriate, conditions imposed to ensure an adequate level of protection.
C	Planning permission should not normally be granted. Where it is considered that permission should be given, for example, because there are no alternative quieter sites available, conditions should be imposed to ensure a commensurate level of protection against noise.
D	Planning permission should normally be refused.

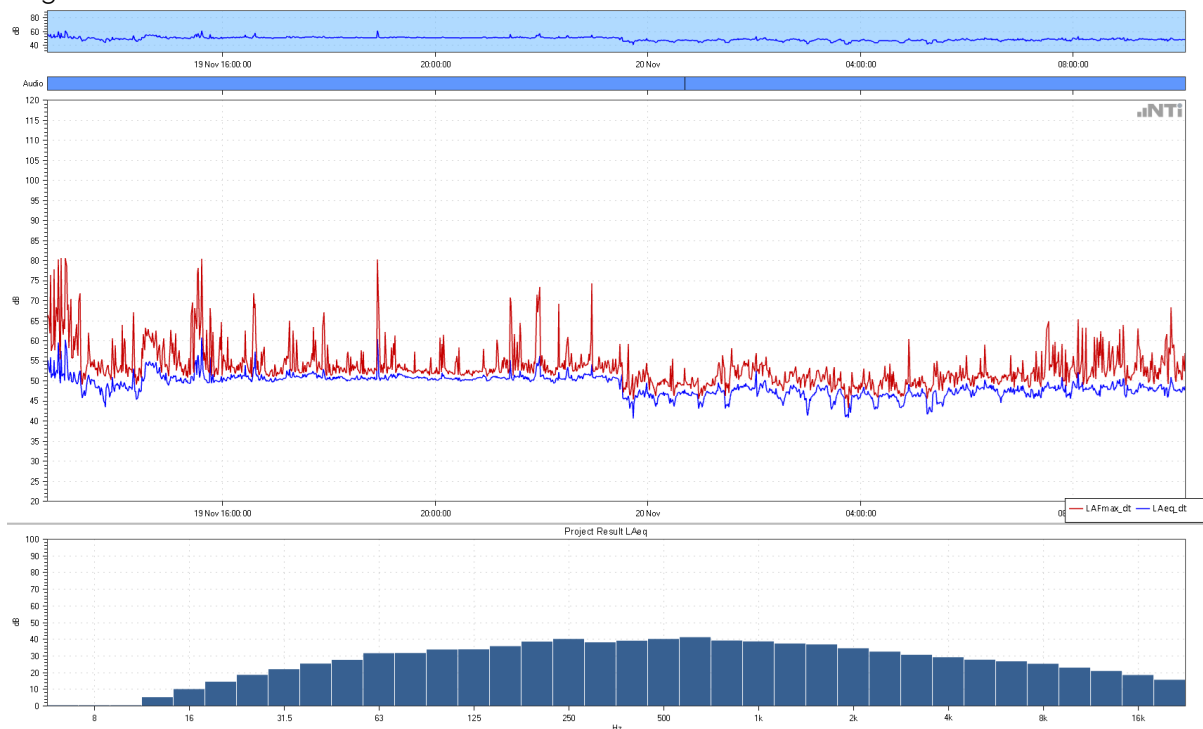
4.0 Results

4.1 – Background Noise – 12.42pm 19/11/25 – 10.06am 20/11/25

Table 2

Time Period	L _{Amax} (Mode)	L _{Aeq1hr} (Mode)	L _{Aeq15min} (Mode)	L _{A90} (Representative)
Day (0700-2300)	80.5dBA	50.5dBA		49.6dBA
Night (2300-0700)	53.1dBA		46.9dBA	43.6dBA

Figure 3



Comments

Some existing industrial noise/plant noise maintaining background noise levels

*based on Appendix C

Time Period	Cloud Cover	Temperature (Celcius)	Presence of fog/snow/ice	Wind Speed (m/s)	Wind Direction
Daytime	1	12	No	1.9	NE
Collection	6	9	No	0.2	N

5.0 Analysis of Results

5.1 Calculated Results

- 5.1.1 The updated specific noise level for the units in the plant area has been calculated using the manufacturers data for sound power on the proposed system as a whole. This has then been entered in the CadnaA noise modelling software so that all aspects of the system can be modelled for noise output. The details in table 3 below have been used for the noise impact model.

Table 3 – sound power values for extraction system

Type	Product	1/1 Octave Sound Power Levels @ 1m from the unit								
		Frequency								
		63 Hz	125 Hz	250 Hz	500 Hz	1 kHz	2 kHz	4 kHz	8kHz	A(dBA)
Insulated Duct Fan	MUB042 500EV	48	67	69	75	79	78	74	66	83
Sileo Axial Fan	AR 450E4	20	42	53	65	68	68	65	60	73
Silencer	LDK 70	-	-5	-7	-19	-24	-23	-15	-10	-27.8

- 5.1.2 Background data was collected at the nearest NSR façade and has been used to compare to the levels in accordance with BS4142:2014.
- 5.1.3 Figure 4 shows the map of the noise propagation emanating from the plant area and extraction point. This does not consider any other noise sources for

Figure 4 – Noise propagation map. Values at residential are based on the highest impact at any height.



- 5.1.4 The nearest window is located below the proposed extraction unit, on the southern-most elevation of the building. This is, however, proposed to be a blocked-up window on the new plans and, as per figure 3, a store room to be behind it. This is therefore not classed as a Noise Sensitive Receptor (NSR) location.
- 5.1.5 The closest residential NSR location/window is the first-floor living room window located in the inset part of the building. as the extraction unit is now on the southern elevation the building itself is acting as a screening object and as such the noise levels at this NSR are only predicted to be 25.4dBA at the centre point of the window.
- 5.1.6 The next closest NSR location is on the adjacent buildings. These provide predicted noise levels of 28dBA and 33dBA respectively.
- 5.1.6 The ducting fan, silencer and main fan unit have all been used as part of the calculation methodology to provide the expected noise propagation from the full unit.
- 5.1.5 With the calculated specific noise level being at a maximum of 33dBA at the closest NSR window, and 28dBA at the next; 33dBA has been used in the calculations in table 5 to assess the noise impact of the units.

Table 5

Measurement Type	Parameter	Result	Comment
Day			
Ambient sound	L_{Aeq}	51dBA	Measured - Source Active
Residual sound level	L_{Aeq5min}	51dBA	Measured 3pm when source inactive
Background sound level	L_{A901hr}	50dBA	Measured 3pm when source inactive
Specific Sound Level	L_{Aeq1hr}	33dBA	Modelled
Acoustic Feature Correction	dBA	+3	No tonal or impulsive noise from plant. Possible on/off element
Rating Level	dBA	36dBA	
Difference of Background vs Rating level	dBA	-14dB	
Chance of Adverse Impact			No Adverse Impact
Night			
Ambient sound	L_{Aeq}	47dBA	Measured - Source Active
Residual sound level	L_{Aeq1hr}	47dBA	Measured 3pm when source inactive
Background sound level	L_{A901hr}	44dBA	Measured at NSR- Source not present
Specific Sound Level	L_{Aeq1hr}	33dBA	Modelled
Acoustic Feature Correction	dBA	+3	No tonal or impulsive noise from plant. Possible on/off element
Rating Level	dBA	36dBA	
Difference of Background vs Rating level	dBA	-8dB	
Chance of Adverse Impact			Low Chance of Adverse Impact

6.0 Conclusion and Further Comments

6.1 Discussion of Levels

- 6.1.1 The specific noise level of the condenser and extraction units are below the values, in accordance with BS4142:2014+A1:2019, for there to be anything more than a low chance of adverse impact expected on the surrounding residential noise sensitive receptors. The night-time period was predicted to be 8dB below the background level with the daytime periods being 14dBA below background. Both of these are well below the required levels in accordance with BS4142:2014.
- 6.1.2 With the moving of the extraction unit to the Southern-most façade there are no longer any visual concerns for the residents. The previous assessment had the extraction system in front of a residential window; which has been corrected in

6.2 Mitigation Measures

- 6.2.1 No additional mitigation measures are required for the site.

7.0 Credentials

Name	Title	Credentials
James Flitton BSc AMIOA	Acoustic Consultant	IOA Diploma in Acoustics & Noise Control
		Associate Member Institute of Acoustics
		Affiliate Member of IDE
		CSCS Professionally Qualified person
Signed		

Appendix A – Acoustic Terminology

Parameter	Description
Ambient Noise Level	The totally encompassing sound in a given situation at a given time, usually composed of a sound from many sources both distant and near ($L_{Aeq,T}$).
Decibel (dB)	A scale for comparing the ratios of two quantities, including sound pressure and sound power. The difference in level between two sounds s_1 and s_2 is given by $20 \log_{10} (s_1/s_2)$. The decibel can also be used to measure absolute quantities by specifying a reference value that fixes one point on the scale. For sound pressure, the reference value is $20\mu\text{Pa}$. The threshold of normal hearing is in the region of 0 dB and 140 dB is the threshold of pain. A change of 1 dB is only perceptible under controlled conditions.
dB(A), L_{Ax}	Decibels measured on a sound level meter incorporating a frequency weighting (A weighting) which differentiates between sounds of different frequency (pitch) in a similar way to the human ear. Measurements in dB(A) broadly agree with people's assessment of loudness. A change of 3 dB(A) is the minimum perceptible under normal conditions, and a change of 10 dB(A) corresponds roughly to halving or doubling the loudness of a sound. The background noise in a living room may be about 30 dB(A); normal conversation about 60 dB(A) at 1 metre; heavy road traffic about 80 dB(A) at 10 metres; the level near a pneumatic drill about 100 dB(A).
Fast Time Weighting	Setting on sound level meter, denoted by a subscript F, that determines the speed at which the instrument responds to changes in the amplitude of any measured signal. The fast time weighting can lead to higher values than the slow time weighting when rapidly changing signals are measured. The average time constant for the fast response setting is 0.125 (1/8) seconds.
Free-field	Sound pressure level measured outside, far away from reflecting surfaces (except the ground), usually taken to mean at least 3.5 metres
Façade	Sound pressure level measured at a distance of 1 metre in front of a large sound reflecting object such as a building façade.
$L_{Aeq,T}$	A noise level index called the equivalent continuous noise level over the time period T. This is the level of a notional steady sound that would contain the same amount of sound energy as the actual, possibly fluctuating, sound that was recorded.
$L_{max,T}$	A noise level index defined as the maximum noise level recorded during a noise event with a period T. L_{max} is sometimes used for the assessment of occasional loud noises, which may have little effect on the overall L_{eq} noise level but will still affect the noise environment. Unless described otherwise, it is measured using the 'fast' sound level meter response.
$L_{10,T}$	A noise level index. The noise level exceeded for 10% of the time over the period T. L_{10} can be considered to be the "average maximum" noise level. Generally used to describe road traffic noise. $L_{A10,18h}$ is the A-weighted arithmetic average of the 18 hourly $L_{A10,1h}$ values from 06:00-24:00.
$L_{90,T}$	A noise level index. The noise level exceeded for 90% of the time over the period T. Generally used to describe background noise level.

Appendix B – Survey Instrumentation

Type	Manufacturer	Model	Serial Number	Last Cal	Cal Due
SLM	NTi	XL2-TA	A2A-18475-E0	12/11/2024	12/11/2026
Pre-amp	NTi	MA220	9378	12/11/2024	12/11/2026
Microphone	NTi	MC230A	A19093	12/11/2024	12/11/2026
Calibrator	NTi	CAL2000	20850	21/07/2025	21/07/2026

Appendix C – Weather Conditions Chart Used

Weather Conditions				
Measurement Location	Date/Time	Description	Beginning of Survey	End of Survey
		Temperature:		
Cloud Cover Symbol Scale in oktas (eighths)  0 Sky completely clear  1  2  3  4 Sky half cloudy  5  6  7  8 Sky completely cloudy  (9) Sky obstructed from view	Precipitation:			
	Cloud cover (oktas - see guide)			
	Presence of fog/snow/ice			
	Presence of damp roads/wet ground			
	Wind Speed (m/s)			
	Wind Direction			
	Conditions that may cause temperature inversion (i.e. calm nights with no cloud)			

Appendix D – CadnaA Calculation Sheet

Receiver
Name: NSR 1
ID:
X: 30441686.56 m
Y: 5723662.16 m
Z: 5.50 m

Point Source, ISO 9613, Name: "", ID: ""																			
Nr.	X	Y	Z	Refl.	DEN	Freq.	Lw	I/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	dB	dB	dB	dB	dB	dB	dB	dB	dB	dB
1	0441687.92	5723654.58	7.00	0	DEN	32	-39.4	0.0	0.0	0.0	0.0	28.9	0.0	-3.0	0.0	0.0	4.0	0.0	0.0
1	0441687.92	5723654.58	7.00	0	DEN	63	21.8	0.0	0.0	0.0	0.0	28.9	0.0	-3.0	0.0	0.0	4.6	0.0	0.0
1	0441687.92	5723654.58	7.00	0	DEN	125	45.9	0.0	0.0	0.0	0.0	28.9	0.0	0.7	0.0	0.0	4.8	0.0	0.0
1	0441687.92	5723654.58	7.00	0	DEN	250	53.4	0.0	0.0	0.0	0.0	28.9	0.0	0.1	0.0	0.0	5.8	0.0	0.0
1	0441687.92	5723654.58	7.00	0	DEN	500	52.8	0.0	0.0	0.0	0.0	28.9	0.0	0.0	0.0	0.0	7.1	0.0	0.0
1	0441687.92	5723654.58	7.00	0	DEN	1000	55.0	0.0	0.0	0.0	0.0	28.9	0.0	0.0	0.0	0.0	8.8	0.0	0.0
1	0441687.92	5723654.58	7.00	0	DEN	2000	56.2	0.0	0.0	0.0	0.0	28.9	0.1	0.0	0.0	0.0	10.9	0.0	0.0
1	0441687.92	5723654.58	7.00	0	DEN	4000	60.0	0.0	0.0	0.0	0.0	28.9	0.3	0.0	0.0	0.0	13.2	0.0	0.0
1	0441687.92	5723654.58	7.00	0	DEN	8000	54.9	0.0	0.0	0.0	0.0	28.9	0.9	0.0	0.0	0.0	15.7	0.0	0.0

Receiver
Name: NSR 2
ID:
X: 30441679.46 m
Y: 5723650.41 m
Z: 5.00 m

Point Source, ISO 9613, Name: "", ID: ""																			
Nr.	X	Y	Z	Refl.	DEN	Freq.	Lw	I/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	dB	dB	dB	dB	dB	dB	dB	dB	dB	dB
2	0441687.92	5723654.58	7.00	0	DEN	32	-39.4	0.0	0.0	0.0	0.0	30.6	0.0	-3.0	0.0	0.0	0.0	0.0	0.0
2	0441687.92	5723654.58	7.00	0	DEN	63	21.8	0.0	0.0	0.0	0.0	30.6	0.0	-3.0	0.0	0.0	0.0	0.0	0.0
2	0441687.92	5723654.58	7.00	0	DEN	125	45.9	0.0	0.0	0.0	0.0	30.6	0.0	0.8	0.0	0.0	0.0	0.0	0.0
2	0441687.92	5723654.58	7.00	0	DEN	250	53.4	0.0	0.0	0.0	0.0	30.6	0.0	0.1	0.0	0.0	0.0	0.0	0.0
2	0441687.92	5723654.58	7.00	0	DEN	500	52.8	0.0	0.0	0.0	0.0	30.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0441687.92	5723654.58	7.00	0	DEN	1000	55.0	0.0	0.0	0.0	0.0	30.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2	0441687.92	5723654.58	7.00	0	DEN	2000	56.2	0.0	0.0	0.0	0.0	30.6	0.1	0.0	0.0	0.0	0.0	0.0	0.0
2	0441687.92	5723654.58	7.00	0	DEN	4000	60.0	0.0	0.0	0.0	0.0	30.6	0.3	0.0	0.0	0.0	0.0	0.0	0.0
2	0441687.92	5723654.58	7.00	0	DEN	8000	54.9	0.0	0.0	0.0	0.0	30.6	1.1	0.0	0.0	0.0	0.0	0.0	0.0

Receiver
Name: NSR 3
ID:
X: 30441686.37 m
Y: 5723638.37 m
Z: 5.00 m

Point Source, ISO 9613, Name: "", ID: ""																			
Nr.	X	Y	Z	Refl.	DEN	Freq.	Lw	I/a	Optime	K0	Di	Adiv	Aatm	Agr	Afol	Ahous	Abar	Cmet	RL
	(m)	(m)	(m)			(Hz)	dB(A)	dB	dB	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)	(dB)
3	0441687.92	5723654.58	7.00	0	DEN	32	-39.4	0.0	0.0	0.0	0.0	35.3	0.0	-3.0	0.0	0.0	0.0	0.0	0.0
3	0441687.92	5723654.58	7.00	0	DEN	63	21.8	0.0	0.0	0.0	0.0	35.3	0.0	-3.0	0.0	0.0	0.0	0.0	0.0
3	0441687.92	5723654.58	7.00	0	DEN	125	45.9	0.0	0.0	0.0	0.0	35.3	0.0	1.4	0.0	0.0	0.0	0.0	0.0
3	0441687.92	5723654.58	7.00	0	DEN	250	53.4	0.0	0.0	0.0	0.0	35.3	0.0	0.3	0.0	0.0	0.0	0.0	0.0
3	0441687.92	5723654.58	7.00	0	DEN	500	52.8	0.0	0.0	0.0	0.0	35.3	0.0	0.0	0.0	0.0	0.0	0.0	0.0
3	0441687.92	5723654.58	7.00	0	DEN	1000	55.0	0.0	0.0	0.0	0.0	35.3	0.1	0.0	0.0	0.0	0.0	0.0	0.0
3	0441687.92	5723654.58	7.00	0	DEN	2000	56.2	0.0	0.0	0.0	0.0	35.3	0.2	0.0	0.0	0.0	0.0	0.0	0.0
3	0441687.92	5723654.58	7.00	0	DEN	4000	60.0	0.0	0.0	0.0	0.0	35.3	0.5	0.0	0.0	0.0	0.0	0.0	0.0
3	0441687.92	5723654.58	7.00	0	DEN	8000	54.9	0.0	0.0	0.0	0.0	35.3	1.9	0.0	0.0	0.0	0.0	0.0	0.0