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STRUCTURAL CALCULATIONS

For

REAR GARDEN RETAINING WALL

at

**29 OLD ROAD
NEATH
SA11 2BT**

Date: December 2024

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STRUCTURAL DESIGN PHILOSOPHY

The following structural design calculations relate to the construction of a rear garden retaining wall which supports a patio area.

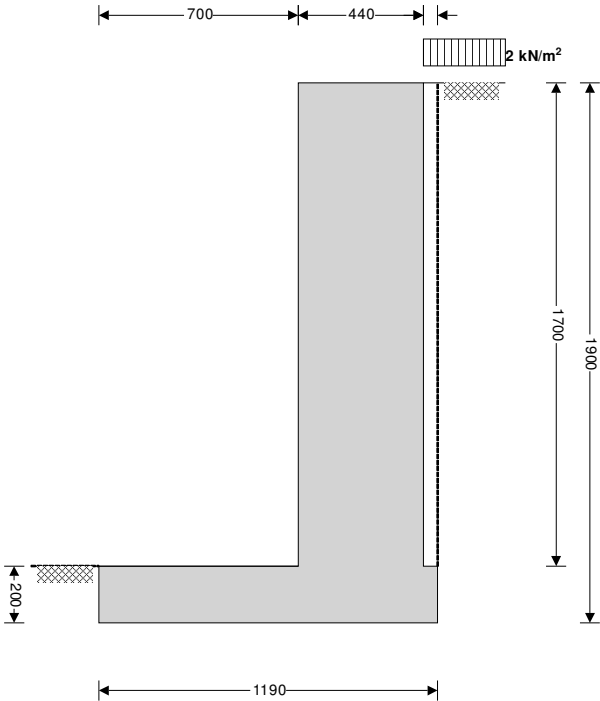
A masonry garage structure is constructed in close proximity to the retaining wall.

No additional surcharges from neighbouring properties are applied to this retaining wall design.

TeklaTedds FAR Structures Ltd Wayside, 30 Brynfield Road, Langland, Swansea, SA3 4SX t: +44 (0)7703 043 608 e:andrew@farstructures.uk	Project	29 Old Road, Neath, SA11 2BT			Job no.	
	Calcs for	Retaining Wall adj Rear Garage			Start page no./Revision	
	Calcs by	Calcs date	Checked by	Checked date	Approved by	Approved date
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RETAINING WALL ANALYSIS (BS 8002:1994)

TEDDS calculation version 1.2.01.08



Wall details

- Retaining wall type
- Height of retaining wall stem
- Thickness of wall stem
- Length of toe
- Length of heel
- Overall length of base
- Thickness of base
- Depth of downstand
- Position of downstand
- Thickness of downstand
- Height of retaining wall
- Depth of cover in front of wall
- Depth of unplanned excavation
- Height of ground water behind wall
- Height of saturated fill above base
- Density of wall construction
- Density of base construction
- Angle of rear face of wall
- Angle of soil surface behind wall
- Effective height at virtual back of wall

Unpropped cantilever

- $h_{\text{stem}} = 1700 \text{ mm}$
- $t_{\text{wall}} = 440 \text{ mm}$
- $l_{\text{toe}} = 700 \text{ mm}$
- $l_{\text{heel}} = 50 \text{ mm}$
- $l_{\text{base}} = l_{\text{toe}} + l_{\text{heel}} + t_{\text{wall}} = 1190 \text{ mm}$
- $t_{\text{base}} = 200 \text{ mm}$
- $d_{\text{ds}} = 0 \text{ mm}$
- $l_{\text{ds}} = 700 \text{ mm}$
- $t_{\text{ds}} = 200 \text{ mm}$
- $h_{\text{wall}} = h_{\text{stem}} + t_{\text{base}} + d_{\text{ds}} = 1900 \text{ mm}$
- $d_{\text{cover}} = 0 \text{ mm}$
- $d_{\text{exc}} = 0 \text{ mm}$
- $h_{\text{water}} = 0 \text{ mm}$
- $h_{\text{sat}} = \max(h_{\text{water}} - t_{\text{base}} - d_{\text{ds}}, 0 \text{ mm}) = 0 \text{ mm}$
- $\gamma_{\text{wall}} = 23.6 \text{ kN/m}^3$
- $\gamma_{\text{base}} = 23.6 \text{ kN/m}^3$
- $\alpha = 90.0 \text{ deg}$
- $\beta = 0.0 \text{ deg}$
- $h_{\text{eff}} = h_{\text{wall}} + l_{\text{heel}} \times \tan(\beta) = 1900 \text{ mm}$

Retained material details

- Mobilisation factor
 - Moist density of retained material
- $M = 1.5$
 $\gamma_m = 18.0 \text{ kN/m}^3$

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Saturated density of retained material $\gamma_s = 21.0 \text{ kN/m}^3$
Design shear strength $\phi' = 27.5 \text{ deg}$
Angle of wall friction $\delta = 21.3 \text{ deg}$

Base material details

Moist density $\gamma_{mb} = 18.0 \text{ kN/m}^3$
Design shear strength $\phi'_b = 27.5 \text{ deg}$
Design base friction $\delta_b = 21.3 \text{ deg}$
Allowable bearing pressure $P_{bearing} = 100 \text{ kN/m}^2$

Using Coulomb theory

Active pressure coefficient for retained material

$K_a = \sin(\alpha + \phi')^2 / (\sin(\alpha)^2 \times \sin(\alpha - \delta) \times [1 + \sqrt{(\sin(\phi' + \delta) \times \sin(\phi' - \beta) / (\sin(\alpha - \delta) \times \sin(\alpha + \beta))}]^2) = 0.326$

Passive pressure coefficient for base material

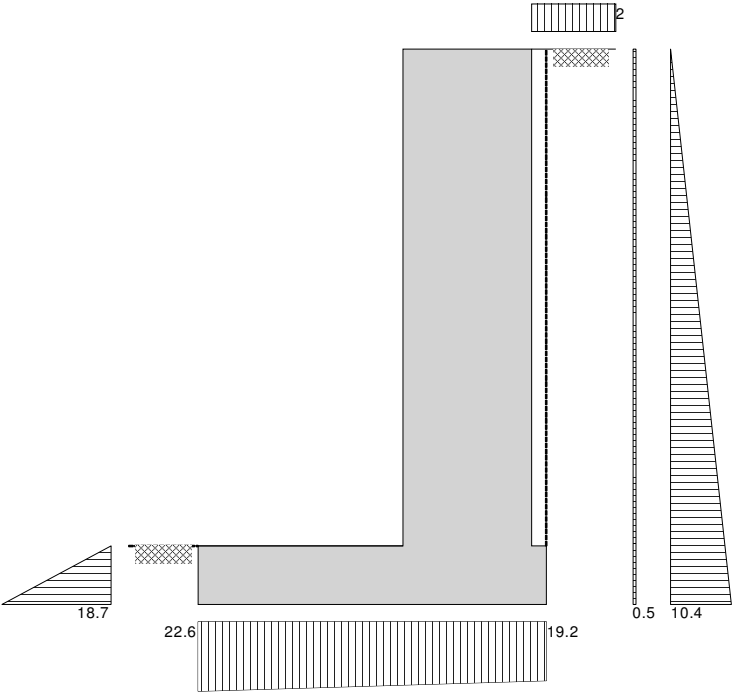
$K_p = \sin(90 - \phi'_b)^2 / (\sin(90 - \delta_b) \times [1 - \sqrt{(\sin(\phi'_b + \delta_b) \times \sin(\phi'_b) / (\sin(90 + \delta_b))}]^2) = 5.571$

At-rest pressure

At-rest pressure for retained material $K_0 = 1 - \sin(\phi') = 0.538$

Loading details

Surcharge load on plan Surcharge = 1.5 kN/m²
Applied vertical dead load on wall $W_{dead} = 0.0 \text{ kN/m}$
Applied vertical live load on wall $W_{live} = 0.0 \text{ kN/m}$
Position of applied vertical load on wall $l_{load} = 0 \text{ mm}$
Applied horizontal dead load on wall $F_{dead} = 0.0 \text{ kN/m}$
Applied horizontal live load on wall $F_{live} = 0.0 \text{ kN/m}$
Height of applied horizontal load on wall $h_{load} = 0 \text{ mm}$



Loads shown in kN/m, pressures shown in kN/m²

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Vertical forces on wall

Wall stem	$w_{wall} = h_{stem} \times t_{wall} \times \gamma_{wall} = 17.7 \text{ kN/m}$
Wall base	$w_{base} = l_{base} \times t_{base} \times \gamma_{base} = 5.6 \text{ kN/m}$
Surcharge	$w_{sur} = \text{Surcharge} \times l_{heel} = 0.1 \text{ kN/m}$
Moist backfill to top of wall	$w_{m_w} = l_{heel} \times (h_{stem} - h_{sat}) \times \gamma_m = 1.5 \text{ kN/m}$
Total vertical load	$W_{total} = w_{wall} + w_{base} + w_{sur} + w_{m_w} = 24.9 \text{ kN/m}$

Horizontal forces on wall

Surcharge	$F_{sur} = K_a \times \cos(90 - \alpha + \delta) \times \text{Surcharge} \times h_{eff} = 0.9 \text{ kN/m}$
Moist backfill above water table	$F_{m_a} = 0.5 \times K_a \times \cos(90 - \alpha + \delta) \times \gamma_m \times (h_{eff} - h_{water})^2 = 9.9 \text{ kN/m}$
Total horizontal load	$F_{total} = F_{sur} + F_{m_a} = 10.7 \text{ kN/m}$

Calculate stability against sliding

Passive resistance of soil in front of wall	$F_p = 0.5 \times K_p \times \cos(\delta_b) \times (d_{cover} + t_{base} + d_{ds} - d_{exc})^2 \times \gamma_{mb} = 1.9 \text{ kN/m}$
Resistance to sliding	$F_{res} = F_p + W_{total} \times \tan(\delta_b) = 11.6 \text{ kN/m}$
PASS - Resistance force is greater than sliding force	

Overturning moments

Surcharge	$M_{sur} = F_{sur} \times (h_{eff} - 2 \times d_{ds}) / 2 = 0.8 \text{ kNm/m}$
Moist backfill above water table	$M_{m_a} = F_{m_a} \times (h_{eff} + 2 \times h_{water} - 3 \times d_{ds}) / 3 = 6.2 \text{ kNm/m}$
Total overturning moment	$M_{ot} = M_{sur} + M_{m_a} = 7.1 \text{ kNm/m}$

Restoring moments

Wall stem	$M_{wall} = w_{wall} \times (l_{toe} + t_{wall} / 2) = 16.2 \text{ kNm/m}$
Wall base	$M_{base} = w_{base} \times l_{base} / 2 = 3.3 \text{ kNm/m}$
Surcharge	$M_{sur_r} = w_{sur} \times (l_{base} - l_{heel} / 2) = 0.1 \text{ kNm/m}$
Moist backfill	$M_{m_r} = (w_{m_w} \times (l_{base} - l_{heel} / 2) + w_{m_s} \times (l_{base} - l_{heel} / 3)) = 1.8 \text{ kNm/m}$
Total restoring moment	$M_{rest} = M_{wall} + M_{base} + M_{sur_r} + M_{m_r} = 21.5 \text{ kNm/m}$

Check stability against overturning

Total overturning moment	$M_{ot} = 7.1 \text{ kNm/m}$
Total restoring moment	$M_{rest} = 21.5 \text{ kNm/m}$
PASS - Restoring moment is greater than overturning moment	

Check bearing pressure

Total moment for bearing	$M_{total} = M_{rest} - M_{ot} = 14.4 \text{ kNm/m}$
Total vertical reaction	$R = W_{total} = 24.9 \text{ kN/m}$
Distance to reaction	$x_{bar} = M_{total} / R = 579 \text{ mm}$
Eccentricity of reaction	$e = \text{abs}((l_{base} / 2) - x_{bar}) = 16 \text{ mm}$
Reaction acts within middle third of base	
Bearing pressure at toe	$p_{toe} = (R / l_{base}) + (6 \times R \times e / l_{base}^2) = 22.6 \text{ kN/m}^2$
Bearing pressure at heel	$p_{heel} = (R / l_{base}) - (6 \times R \times e / l_{base}^2) = 19.2 \text{ kN/m}^2$
PASS - Maximum bearing pressure is less than allowable bearing pressure	

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RETAINING WALL DESIGN (BS 8002:1994)

TEDDS calculation version 1.2.01.08

Ultimate limit state load factors

Dead load factor	$\gamma_{f_d} = 1.4$
Live load factor	$\gamma_{f_l} = 1.6$
Earth and water pressure factor	$\gamma_{f_e} = 1.4$

Factored vertical forces on wall

Wall stem	$W_{wall_f} = \gamma_{f_d} \times h_{stem} \times t_{wall} \times \gamma_{wall} = 24.7 \text{ kN/m}$
Wall base	$W_{base_f} = \gamma_{f_d} \times l_{base} \times t_{base} \times \gamma_{base} = 7.9 \text{ kN/m}$
Surcharge	$W_{sur_f} = \gamma_{f_l} \times \text{Surcharge} \times l_{heel} = 0.1 \text{ kN/m}$
Moist backfill to top of wall	$W_{m_w_f} = \gamma_{f_d} \times l_{heel} \times (h_{stem} - h_{sat}) \times \gamma_m = 2.1 \text{ kN/m}$
Total vertical load	$W_{total_f} = W_{wall_f} + W_{base_f} + W_{sur_f} + W_{m_w_f} = 34.8 \text{ kN/m}$

Factored horizontal at-rest forces on wall

Surcharge	$F_{sur_f} = \gamma_{f_l} \times K_0 \times \text{Surcharge} \times h_{eff} = 2.5 \text{ kN/m}$
Moist backfill above water table	$F_{m_a_f} = \gamma_{f_e} \times 0.5 \times K_0 \times \gamma_m \times (h_{eff} - h_{water})^2 = 24.5 \text{ kN/m}$
Total horizontal load	$F_{total_f} = F_{sur_f} + F_{m_a_f} = 26.9 \text{ kN/m}$
Passive resistance of soil in front of wall	$F_{p_f} = \gamma_{f_e} \times 0.5 \times K_p \times \cos(\delta_b) \times (d_{cover} + t_{base} + d_{ds} - d_{exc})^2 \times \gamma_{mb} = 2.6 \text{ kN/m}$

Factored overturning moments

Surcharge	$M_{sur_f} = F_{sur_f} \times (h_{eff} - 2 \times d_{ds}) / 2 = 2.3 \text{ kNm/m}$
Moist backfill above water table	$M_{m_a_f} = F_{m_a_f} \times (h_{eff} + 2 \times h_{water} - 3 \times d_{ds}) / 3 = 15.5 \text{ kNm/m}$
Total overturning moment	$M_{ot_f} = M_{sur_f} + M_{m_a_f} = 17.8 \text{ kNm/m}$

Restoring moments

Wall stem	$M_{wall_f} = W_{wall_f} \times (l_{toe} + t_{wall} / 2) = 22.7 \text{ kNm/m}$
Wall base	$M_{base_f} = W_{base_f} \times l_{base} / 2 = 4.7 \text{ kNm/m}$
Surcharge	$M_{sur_r_f} = W_{sur_f} \times (l_{base} - l_{heel} / 2) = 0.1 \text{ kNm/m}$
Moist backfill	$M_{m_r_f} = (W_{m_w_f} \times (l_{base} - l_{heel} / 2) + W_{m_s_f} \times (l_{base} - l_{heel} / 3)) = 2.5 \text{ kNm/m}$
Total restoring moment	$M_{rest_f} = M_{wall_f} + M_{base_f} + M_{sur_r_f} + M_{m_r_f} = 30.1 \text{ kNm/m}$

Factored bearing pressure

Total moment for bearing	$M_{total_f} = M_{rest_f} - M_{ot_f} = 12.2 \text{ kNm/m}$
Total vertical reaction	$R_f = W_{total_f} = 34.8 \text{ kN/m}$
Distance to reaction	$x_{bar_f} = M_{total_f} / R_f = 351 \text{ mm}$
Eccentricity of reaction	$e_f = \text{abs}((l_{base} / 2) - x_{bar_f}) = 244 \text{ mm}$

Reaction acts outside middle third of base

Bearing pressure at toe	$p_{toe_f} = R_f / (1.5 \times x_{bar_f}) = 66.3 \text{ kN/m}^2$
Bearing pressure at heel	$p_{heel_f} = 0 \text{ kN/m}^2 = 0 \text{ kN/m}^2$
Rate of change of base reaction	$\text{rate} = p_{toe_f} / (3 \times x_{bar_f}) = 63.00 \text{ kN/m}^2/\text{m}$
Bearing pressure at stem / toe	$p_{stem_toe_f} = \text{max}(p_{toe_f} - (\text{rate} \times l_{toe}), 0 \text{ kN/m}^2) = 22.2 \text{ kN/m}^2$
Bearing pressure at mid stem	$p_{stem_mid_f} = \text{max}(p_{toe_f} - (\text{rate} \times (l_{toe} + t_{wall} / 2)), 0 \text{ kN/m}^2) = 8.3 \text{ kN/m}^2$
Bearing pressure at stem / heel	$p_{stem_heel_f} = \text{max}(p_{toe_f} - (\text{rate} \times (l_{toe} + t_{wall})), 0 \text{ kN/m}^2) = 0 \text{ kN/m}^2$

Design of reinforced concrete retaining wall toe (BS 8002:1994)

Material properties

Characteristic strength of concrete	$f_{cu} = 35 \text{ N/mm}^2$
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Characteristic strength of reinforcement

$$f_y = 500 \text{ N/mm}^2$$

Base details

Minimum area of reinforcement

$$k = 0.13 \%$$

Cover to reinforcement in toe

$$c_{toe} = 40 \text{ mm}$$

Calculate shear for toe design

Shear from bearing pressure

$$V_{toe_bear} = (p_{toe_f} + p_{stem_toe_f}) \times l_{toe} / 2 = 30.9 \text{ kN/m}$$

Shear from weight of base

$$V_{toe_wt_base} = \gamma_{f_d} \times \gamma_{base} \times l_{toe} \times t_{base} = 4.6 \text{ kN/m}$$

Total shear for toe design

$$V_{toe} = V_{toe_bear} - V_{toe_wt_base} = 26.3 \text{ kN/m}$$

Calculate moment for toe design

Moment from bearing pressure

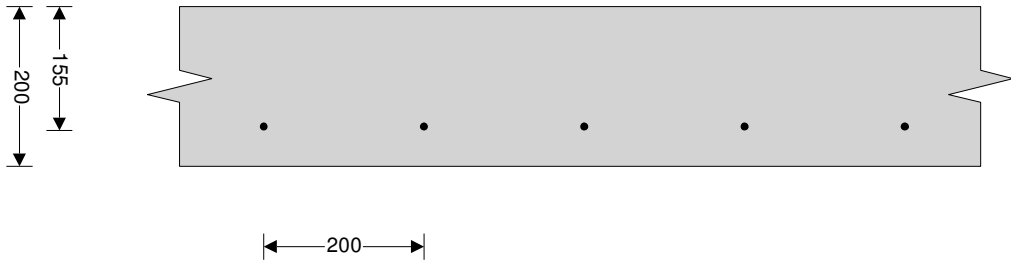
$$M_{toe_bear} = (2 \times p_{toe_f} + p_{stem_mid_f}) \times (l_{toe} + t_{wall} / 2)^2 / 6 = 19.9 \text{ kNm/m}$$

Moment from weight of base

$$M_{toe_wt_base} = (\gamma_{f_d} \times \gamma_{base} \times t_{base} \times (l_{toe} + t_{wall} / 2)^2 / 2) = 2.8 \text{ kNm/m}$$

Total moment for toe design

$$M_{toe} = M_{toe_bear} - M_{toe_wt_base} = 17.1 \text{ kNm/m}$$



Check toe in bending

Width of toe

$$b = 1000 \text{ mm/m}$$

Depth of reinforcement

$$d_{toe} = t_{base} - c_{toe} - (\phi_{toe} / 2) = 155.0 \text{ mm}$$

Constant

$$K_{toe} = M_{toe} / (b \times d_{toe}^2 \times f_{cu}) = 0.020$$

Compression reinforcement is not required

Lever arm

$$z_{toe} = \min(0.5 + \sqrt{(0.25 - (\min(K_{toe}, 0.225) / 0.9))}, 0.95) \times d_{toe}$$

$$z_{toe} = 147 \text{ mm}$$

Area of tension reinforcement required

$$A_{s_toe_des} = M_{toe} / (0.87 \times f_y \times z_{toe}) = 266 \text{ mm}^2/\text{m}$$

Minimum area of tension reinforcement

$$A_{s_toe_min} = k \times b \times t_{base} = 260 \text{ mm}^2/\text{m}$$

Area of tension reinforcement required

$$A_{s_toe_req} = \text{Max}(A_{s_toe_des}, A_{s_toe_min}) = 266 \text{ mm}^2/\text{m}$$

Reinforcement provided

A393 mesh

Area of reinforcement provided

$$A_{s_toe_prov} = 393 \text{ mm}^2/\text{m}$$

PASS - Reinforcement provided at the retaining wall toe is adequate

Check shear resistance at toe

Design shear stress

$$v_{toe} = V_{toe} / (b \times d_{toe}) = 0.170 \text{ N/mm}^2$$

Allowable shear stress

$$v_{adm} = \min(0.8 \times \sqrt{f_{cu}} / 1 \text{ N/mm}^2, 5) \times 1 \text{ N/mm}^2 = 4.733 \text{ N/mm}^2$$

PASS - Design shear stress is less than maximum shear stress

From BS8110:Part 1:1997 – Table 3.8

Design concrete shear stress

$$v_{c_toe} = 0.567 \text{ N/mm}^2$$

$v_{toe} < v_{c_toe}$ - No shear reinforcement required

Design of reinforced concrete retaining wall heel (BS 8002:1994)

Material properties

Characteristic strength of concrete

$$f_{cu} = 35 \text{ N/mm}^2$$

Characteristic strength of reinforcement

$$f_y = 500 \text{ N/mm}^2$$

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Base details

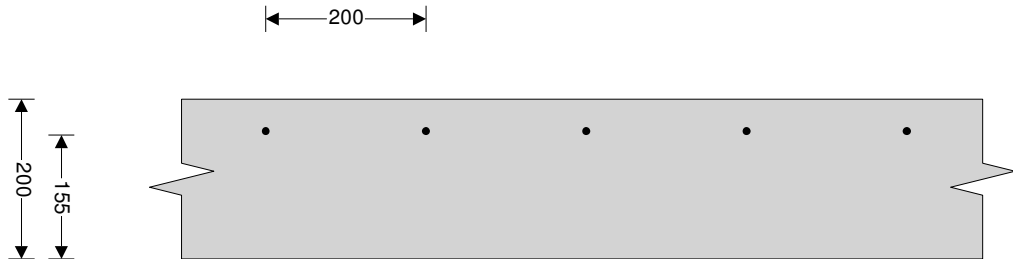
Minimum area of reinforcement $k = 0.13 \%$
Cover to reinforcement in heel $C_{heel} = 40 \text{ mm}$

Calculate shear for heel design

Shear from weight of base $V_{heel_wt_base} = \gamma_{fd} \times \gamma_{base} \times l_{heel} \times t_{base} = 0.3 \text{ kN/m}$
Shear from weight of moist backfill $V_{heel_wt_m} = w_{m_w_f} = 2.1 \text{ kN/m}$
Shear from surcharge $V_{heel_sur} = w_{sur_f} = 0.1 \text{ kN/m}$
Total shear for heel design $V_{heel} = V_{heel_wt_base} + V_{heel_wt_m} + V_{heel_sur} = 2.6 \text{ kN/m}$

Calculate moment for heel design

Moment from weight of base $M_{heel_wt_base} = (\gamma_{fd} \times \gamma_{base} \times t_{base} \times (l_{heel} + t_{wall} / 2)^2 / 2) = 0.2 \text{ kNm/m}$
Moment from weight of moist backfill $M_{heel_wt_m} = w_{m_w_f} \times (l_{heel} + t_{wall}) / 2 = 0.5 \text{ kNm/m}$
Moment from surcharge $M_{heel_sur} = w_{sur_f} \times (l_{heel} + t_{wall}) / 2 = 0 \text{ kNm/m}$
Total moment for heel design $M_{heel} = M_{heel_wt_base} + M_{heel_wt_m} + M_{heel_sur} = 0.8 \text{ kNm/m}$



Check heel in bending

Width of heel $b = 1000 \text{ mm/m}$
Depth of reinforcement $d_{heel} = t_{base} - C_{heel} - (\phi_{heel} / 2) = 155.0 \text{ mm}$
Constant $K_{heel} = M_{heel} / (b \times d_{heel}^2 \times f_{cu}) = 0.001$
Compression reinforcement is not required
Lever arm $Z_{heel} = \min(0.5 + \sqrt{(0.25 - (\min(K_{heel}, 0.225) / 0.9))}, 0.95) \times d_{heel}$
 $Z_{heel} = 147 \text{ mm}$
Area of tension reinforcement required $A_{s_heel_des} = M_{heel} / (0.87 \times f_y \times Z_{heel}) = 12 \text{ mm}^2/\text{m}$
Minimum area of tension reinforcement $A_{s_heel_min} = k \times b \times t_{base} = 260 \text{ mm}^2/\text{m}$
Area of tension reinforcement required $A_{s_heel_req} = \text{Max}(A_{s_heel_des}, A_{s_heel_min}) = 260 \text{ mm}^2/\text{m}$
Reinforcement provided **A393 mesh**
Area of reinforcement provided $A_{s_heel_prov} = 393 \text{ mm}^2/\text{m}$

PASS - Reinforcement provided at the retaining wall heel is adequate

Check shear resistance at heel

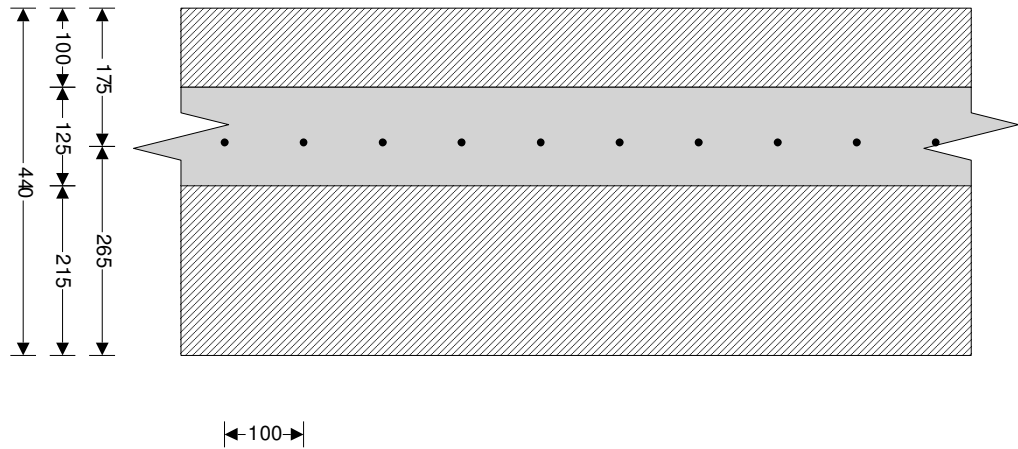
Design shear stress $v_{heel} = V_{heel} / (b \times d_{heel}) = 0.017 \text{ N/mm}^2$
Allowable shear stress $v_{adm} = \min(0.8 \times \sqrt{f_{cu}} / 1 \text{ N/mm}^2, 5) \times 1 \text{ N/mm}^2 = 4.733 \text{ N/mm}^2$
PASS - Design shear stress is less than maximum shear stress

From BS8110:Part 1:1997 – Table 3.8

Design concrete shear stress $v_{c_heel} = 0.567 \text{ N/mm}^2$
 $v_{heel} < v_{c_heel}$ - No shear reinforcement required

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Design of cavity reinforced masonry retaining wall stem - BS5628-2:2000



Wall details

Thickness of outer leaf of wall
Thickness of inner leaf of wall
Thickness of reinforced cavity
Depth of stem reinforcement

$t_{\text{outer}} = 100 \text{ mm}$
 $t_{\text{inner}} = 215 \text{ mm}$
 $t_{\text{cavity}} = t_{\text{wall}} - t_{\text{outer}} - t_{\text{inner}} = 125 \text{ mm}$
 $d_{\text{stem}} = 175 \text{ mm}$

Masonry details

Masonry type
Compressive strength of units
Mortar designation
Category of manufacturing control of units
Partial safety factor for material strength

Aggregate concrete blocks no voids
 $p_{\text{unit}} = 7.3 \text{ N/mm}^2$
(ii)
Category I
 $\gamma_{\text{mm}} = 2.0$

Characteristic compressive strength of masonry

Least horizontal dimension of masonry units
Height of masonry units
Ratio of height to least horizontal dimension
From BS5628:2 Table 3d, mortar ii
Characteristic compressive strength

$b_{\text{unit}} = 100.0 \text{ mm}$
 $h_{\text{unit}} = 215.0 \text{ mm}$
 $\text{ratio} = h_{\text{unit}} / b_{\text{unit}} = 2.2$
 $f_k = 6.4 \text{ N/mm}^2$

Factored horizontal at-rest forces on stem

Surcharge
Moist backfill above water table

$F_{s_sur_f} = \gamma_{t_j} \times K_0 \times \text{Surcharge} \times (h_{\text{eff}} - t_{\text{base}} - d_{\text{ds}}) = 2.2 \text{ kN/m}$
 $F_{s_m_a_f} = 0.5 \times \gamma_{t_e} \times K_0 \times \gamma_m \times (h_{\text{eff}} - t_{\text{base}} - d_{\text{ds}} - h_{\text{sat}})^2 = 19.6 \text{ kN/m}$

Calculate shear for stem design

Shear at base of stem

$V_{\text{stem}} = F_{s_sur_f} + F_{s_m_a_f} = 21.8 \text{ kN/m}$

Calculate moment for stem design

Surcharge
Moist backfill above water table
Total moment for stem design

$M_{s_sur} = F_{s_sur_f} \times (h_{\text{stem}} + t_{\text{base}}) / 2 = 2.1 \text{ kNm/m}$
 $M_{s_m_a} = F_{s_m_a_f} \times (2 \times h_{\text{sat}} + h_{\text{eff}} - d_{\text{ds}} + t_{\text{base}} / 2) / 3 = 13.1 \text{ kNm/m}$
 $M_{\text{stem}} = M_{s_sur} + M_{s_m_a} = 15.2 \text{ kNm/m}$

Check maximum design moment for wall stem

Width of wall
Maximum design moment

$b = 1000 \text{ mm/m}$
 $M_{d_stem} = 0.4 \times f_k \times b \times d_{\text{stem}}^2 / \gamma_{\text{mm}} = 39.2 \text{ kNm/m}$

PASS - Applied moment is less than maximum design moment

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Check wall stem in bending

Moment of resistance factor

$Q = M_{stem} / d_{stem}^2 = 0.495 \text{ N/mm}^2$

$Q = 2 \times c \times (1 - c) \times f_k / \gamma_{mm}$

Lever arm factor

$c = 0.916$

Lever arm

$Z_{stem} = \min(0.95, c) \times d_{stem} = 160.2 \text{ mm}$

Area of tension reinforcement required

$A_{s_stem_des} = M_{stem} \times \gamma_{ms} / (f_y \times Z_{stem}) = 218 \text{ mm}^2/\text{m}$

Minimum area of tension reinforcement

$A_{s_stem_min} = k \times b \times t_{wall} = 572 \text{ mm}^2/\text{m}$

Area of tension reinforcement required

$A_{s_stem_req} = \text{Max}(A_{s_stem_des}, A_{s_stem_min}) = 572 \text{ mm}^2/\text{m}$

Reinforcement provided

B785 mesh

Area of reinforcement provided

$A_{s_stem_prov} = \pi \times \phi_{stem}^2 / (4 \times s_{stem}) = 785 \text{ mm}^2/\text{m}$

PASS - Reinforcement provided at the retaining wall stem is adequate

Check shear resistance at wall stem

Design shear stress

$v_{stem} = V_{stem} / (b \times d_{stem}) = 0.125 \text{ N/mm}^2$

Basic characteristic shear strength of masonry

$f_{vbas} = \min[0.35 + (17.5 \times A_{s_stem_prov} / (b \times d_{stem})), 0.7] \times 1 \text{ N/mm}^2$

$f_{vbas} = 0.429 \text{ N/mm}^2$

Shear span

$a = M_{stem} / V_{stem} = 695.2 \text{ mm}$

Characteristic shear strength of masonry

$f_v = \text{Min}(f_{vbas} \times \max(2.5 - 0.25 \times (a / d_{stem}), 1), 1.75 \text{ N/mm}^2)$

$f_v = 0.646 \text{ N/mm}^2$

Allowable shear stress

$v_{adm} = f_v / \gamma_{mv} = 0.323 \text{ N/mm}^2$

PASS - Design shear stress is less than maximum shear stress

Check limiting dimensions

Limiting span/effective depth ratio

$ratio_{max} = 18.00$

Actual span/effective depth ratio

$ratio_{act} = (h_{stem} + d_{stem} / 2) / d_{stem} = 10.21$

PASS - Span to depth ratio is acceptable

Axial load check

Factored axial load on wall

$N_{wall} = ([t_{wall} \times h_{stem} \times \gamma_{wall} + W_{dead}] \times \gamma_{f_d}) + (W_{live} \times \gamma_{f_l}) = 24.7 \text{ kN/m}$

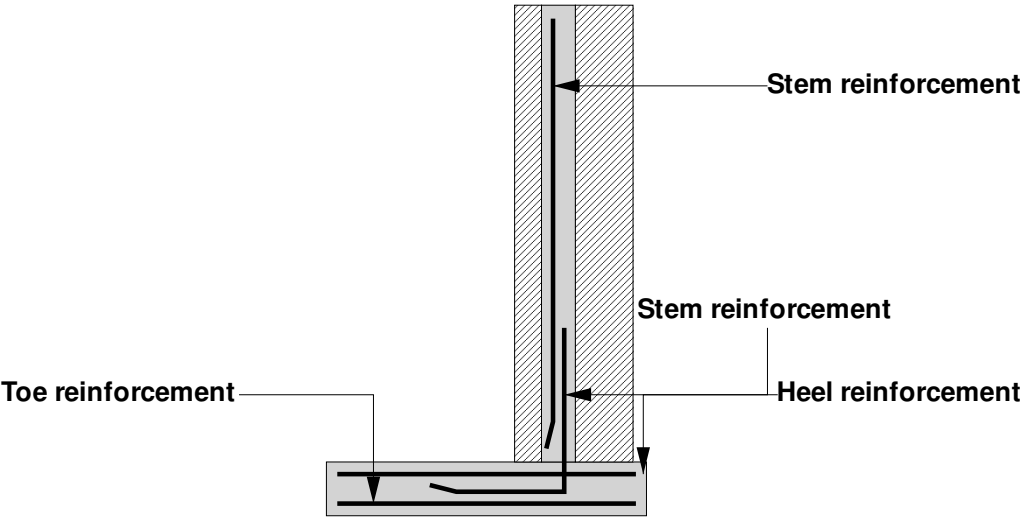
Limiting axial load

$N_{limit} = 0.1 \times f_k \times t_{wall} = 281.6 \text{ kN/m}$

Applied axial load may be ignored - calculations valid

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Indicative retaining wall reinforcement diagram



Toe mesh - A393 - (393 mm²/m)
 Heel mesh - A393 - (393 mm²/m)
 Stem mesh - B785 - (785 mm²/m)